

Determination of Suitable Anti-Scaling Agent to Inhibit Scale Formation of Water Processed in Coal Power Plant System

Elvis Fosso-Kankeu*, Christopher.E. Brider, Johannes Redelinghuys, Gerhard Gericke, Nico Lemmer and Frans Waanders

Abstract— Increasing pollution and scarcity of fresh water have prompted the need to develop and implement effective strategies to treat wastewater and reduce water usage. One such a strategy is to recirculate waste water in a power plant, but this strategy necessitates treatment. The considered water contains high levels of scale forming ions. Scale formation needs to be controlled, to practically increase the feasibility of recirculation processes. The selected test method to determine anti-scalant induction times is found to be inefficient and an improvement on the current method is proposed, and the possible causes for the inefficiency of the selected induction time test method highlighted. The main finding in this study was observed at 75°C as the anti-scalant PBTC performed better than ATMP; the former exhibiting longer induction time in reverse osmosis reject water.

Keywords—Anti-scalant, Scale, PBTC (2-Phosphonobutane-1,2,4-Tricarboxylic Acid), AMTP (Amino Trimethylene Phosphonic Acid), Cooling water.

I. INTRODUCTION

Water is the single most important resource to sustain biological life. Due to the importance of water, the conservation thereof is becoming more significant. “The 2015/16 drought was the most severe in 23 years, leading to all South Africa’s provinces, except Gauteng, being declared disaster areas” [1]. Coupled to that is the growing industrial pollution which put more pressure on the limited fresh water resource [2 - 17]. The high concentration of scale forming agents in such polluted water may pose significant problems when considering treatment through membrane or thermal technology. Scale build up in heat transfer units such as heat exchangers and membrane filters causes a decrease in the efficiency of heat transfer in a chemical or power plants cooling water system [18 - 20]. Maintenance to bring the

equipment back up to working efficiency, needs to continuously be implemented and during maintenance, production could decrease and economic factors are negatively influenced. If membranes and other equipment work less efficiently due to scale build up during operation, more water is wasted which could have been used as supply for drinking water or any other necessary use.

The determining factors of water shortages, will not only be determined by current main causes such as droughts but will also be determined by increased population growth. [21] “The Water Research Commission (WRC) emphasized the need for water resource managers and planners to think outside the box for unconventional water sources, since water shortages stretch far beyond a drought. The South African legislation and regulation forbids industries around the country from discharging waste water in the environment without prior treatment. South African power plants can use the produced waste water more efficiently by recirculation thereof back into the cooling system.

The possible use of process units; which could form part of a cooling water reuse system such as the use of multi-effect distillator to produce water with a sufficient quality from a Reverse-osmosis (RO) reject effluent, encounters the problem of scaling (mostly due to calcium carbonate and calcium sulphate in solutions) which can affect heat exchange capacity [18]. Furthermore, scale formation on reverse osmosis membranes can significantly reduce the water flux through the membrane, necessitating frequent and costly maintenance. Scale forms due to changes in the physical conditions of the water. Anti-scaling agents work to inhibit this formation by interfering with the scale forming mechanism; by interfering with clustering, nucleation, crystal growth, or flocculation. Scaling ions form clusters, thereafter these clusters can grow into crystal structures. Many anti-scaling agent mechanisms have been proposed. One of the more general proposed mechanisms is that anti-scaling agents act to inhibit the onset of nucleation of scaling ions or by inhibiting the crystal growth. [22] propose two kinetic models by which anti-scaling inhibition takes place. Generally anti-scalants do not eliminate the scaling constituents or its tendency; instead they delay the onset crystallization (nucleation phase of crystallization) or retard the growth of mineral salt crystals (growth phase of

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Christopher E. Brider is currently studying post-grad degree at North-West University, Potchefstroom, South Africa (e-mail: chris.brider@gmail.com).

Elvis Fosso-Kankeu is with North-West University, Potchefstroom, South Africa. (e-mail: 24838616@nwu.ac.za).

Frans Waanders is with North-West University, Potchefstroom, South Africa.

Gerhard Gericke is currently an employee at the research department of Eskom Rosherville, South Africa, (e-mail: GerickG@eskom.co.za).

crystallization) [22]. An example of an anti-scaling agent is polyaspartic acid, which is non-toxic, does not contain phosphorous and shows good biodegradability and the carboxylic, hydroxylic and acylamino functional groups in its chemical structure are what give this chemical its scale inhibiting properties, but does not show great inhibiting performance [23]. The functional groups having certain affinities to different scale forming substances.

By adding a suitable anti-scaling agent or a combination of more than one anti-scaling agent, the industry in turn could decrease maintenance costs on relevant equipment [26, 27]. A suitable method for determining anti-scalant induction time needs to be established and factors unaccounted for need to be taken into consideration while modifying the current method. Data from the current method of anti-scalant testing are analyzed and the possible cause of the failure of the method suggested.

II. EXPERIMENTAL

A. Materials and Methods

Sampling location was at Grootvlei coal fired power plant, where two water streams were sampled; cooling water blowdown/bleed off stream (CW-Blowdown), with a conductivity of 1.976 mS/cm and pH 7.4 and RO-reject stream, with a conductivity of 1.076 mS/cm and pH 7.8. The water was stored in a fridge under a dark cover, eliminating light and decrease the chances of pre-mature precipitation of CaCO_3 . Samples were placed at room temperature for a day before use thereof.

A synthetic water sample (control) was prepared by dissolving salts with a concentration of $0.005\text{mol/dm}^3 \text{CaCl}_2$ and $0.005\text{mol/dm}^3 \text{Ca}(\text{HCO}_3)_2$ in demineralized water. The pH of the control water was 7.5.

500 mL of the RO reject and cooling water blowdown samples were spiked with 0.105 g $\text{Ca}(\text{HCO}_3)_2$ and 0.138 g CaCl_2 ; amounting to the same content as the control solution. The synthetic control sample was used to investigate the difference between the sampled water (CW-blowdown and RO-reject), and the synthetic water sample and to note if the minerals in the sampled water interacts with the scale forming mechanism in any way.

B. ICP-OES Analysis

An ICP analysis using ICP Expert II, Agilent Technologies 720 ICP-OES (Agilent Technologies, USA) was performed to determine the concentration of calcium present in the two sampled waters.

C. EDTA Titration

Establishment of the amount of total hardness (sum of magnesium and calcium hardness as CaCO_3) and calcium hardness as CaCO_3 was achieved by an EDTA titration.

D. Static Induction Test

A static induction test was performed in order to determine the induction time of two anti-scalants. PBTC (2-

Phosphonobutane-1,2,4-Tricarboxylic Acid) and AMTP (Amino Trimethylene Phosphonic Acid)

Anti-scalants were dosed into both samples, including the control solution. The anti-scalants were evaluated at temperatures of 25°C, 40°C and 75°C.

A dosage concentration of anti-scalant was selected by using a modelling program (French Creek Software®). After experimentation of the modeled dosage, final dosages of 0.2 ppm of PBTC and ATMP were chosen for the RO-reject sample and 0.1 ppm of PBTC and ATMP was chosen for the cooling water blowdown sample as well as a control solution, as these dosages showed a drop in conductivity within a reasonable time. RO-reject and CW-blowdown were spiked with $0.005\text{mol/dm}^3 \text{CaCl}_2$ and $0.005\text{mol/dm}^3 \text{Ca}(\text{HCO}_3)_2$

An Arduino Uno micro-controller was used to measure the resistivity of the samples over time by means of a voltage divider calculation:

$$R_{\text{water}} = \frac{V_{\text{out}} R_1}{V_s - V_{\text{out}}} \quad (1)$$

Where R_{water} is the resistivity of the water, V_{out} is the resistivity of the voltage read at the sensor and V_s is the output voltage of the source (Arduino). V_s is 5V, with R_1 a chosen voltage of 1740 Ω . The resistance is chosen such that the sensor voltage can stay within the range of 0-5 V.

Two copper wires were placed in the water samples. Stirring was achieved by using a jar test stirrer, which stirs the solution at 60 rpm. Six jars, containing 500 mL each of the water samples were tested simultaneously, consisting of two blank samples, two ATMP dosed samples and two PBTC dosed samples. The samples were heated up by means of circulating hot water on a tray containing the six jars.

The measured resistivity was converted to conductivity, where data was then treated with a Savitzky-Golay smoothing algorithm, to eliminate noise from the data.

III. RESULTS AND DISCUSSION

A. Sample Pre-Analysis

The calcium content of the samples determined using ICP-OES was 83.61ppm in the CW-Blowdown sample and 170.4 ppm in the RO-reject sample.

An EDTA titration resulted in a total hardness as CaCO_3 of 275.08 mg CaCO_3/L , of which the Calcium hardness was determined as 160.46 mg CaCO_3/L , for the CW-Blowdown sample, whereas the RO-reject sample contained 558 mg CaCO_3/L , of which the Calcium hardness was 348 mg CaCO_3/L

B. Static Induction Test at 25°C

Note: Conductivities are not accurate due to noise, polarization on the wire probes and electro-magnetic induction present from the use of an Arduino set-up, the changes in conductivity can however be considered for determining an induction time in the case of this experiment.

Anti-scalants (PBTC & ATMP) were evaluated at 25°C. The first gradual increase in conductivity was due to the increase of energy in the form of heat, as the samples were heated from ambient temperature to 25°C in this case. Ions moved more readily upon elevated temperature, thereby increasing conductivity. A decrease in conductivity occurs when the ion content of the water decrease, which is the case when scale precipitates/depositions from the water. Experimental runs of 12 hours were considered for 25°C, 6 hours for 40°C and 2 hours for 75°C

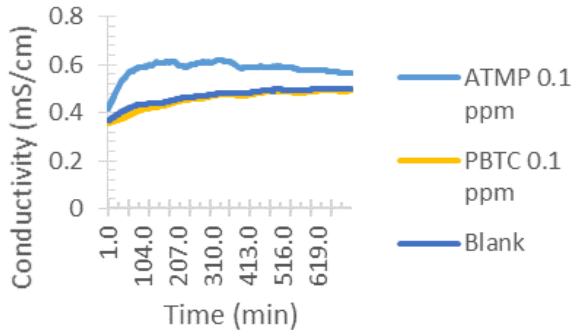


Fig 1: Conductivity over time (Control solution 25°C)

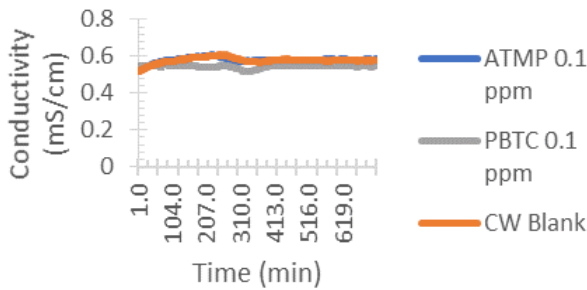


Fig 2: Conductivity over time (CW sample 25°C)

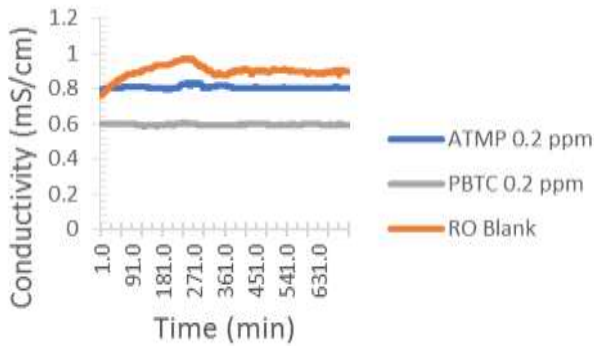


Fig 3: Conductivity over time (RO sample 25°C)

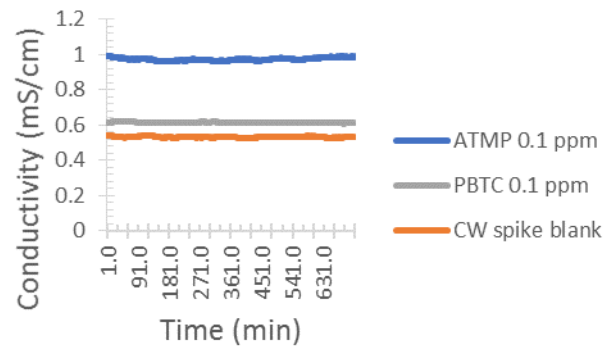


Fig 4: Conductivity over time (CW spike sample 25°C)

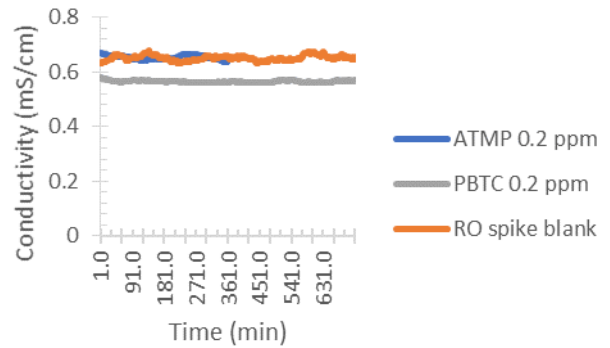


Fig 5: Conductivity over time (RO spike sample 25°C)

As can be seen from Figures 1-5, there was no significant change in conductivity for any of the considered samples at room temperature. At room temperature conditions and for the time considered, the samples are under saturated with potential scale forming ions (Ca^{2+} and CO_3^{2-}).

C. Static induction test at 40°C

The initial increase in conductivity observed at 40°C was higher than that noticed at 25°C. The effect of temperature on conductivity, was therefore observed.

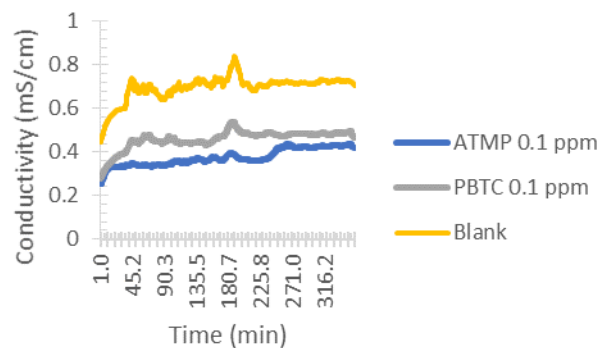


Fig 6: Conductivity over time (Control solution 40°C)

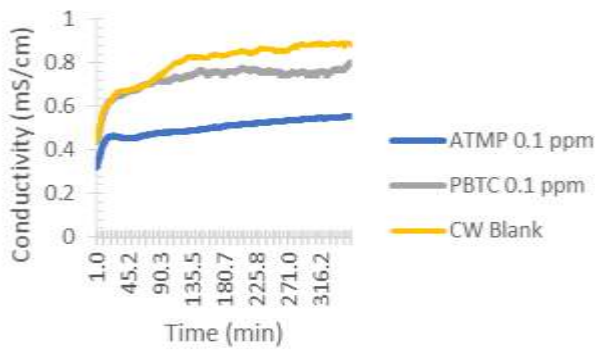


Fig 7: Conductivity over time (CW sample 40°C)

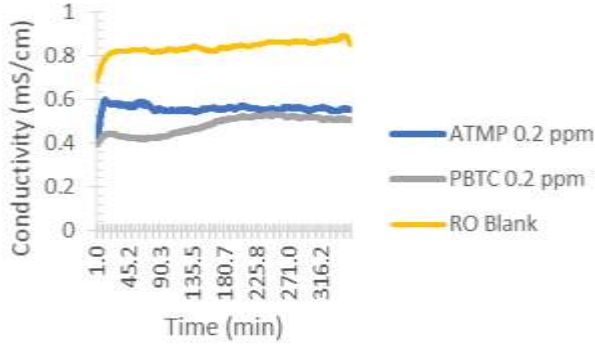


Fig 8: Conductivity over time (RO sample 40°C)

In Fig 7 and Fig 8 it seems that the rate of change in conductivity decreases during the initial increase in temperature of the water, which could be indicative of the occurrence of precipitation, which could be the case for Fig 7 as this behavior occurs on the Blank sample, but for Fig 8 the behavior occurs in the PBTC dosed sample and not in the blank sample, which is inconsistent and counter intuitive to the idea that anti-scalants increase induction time.

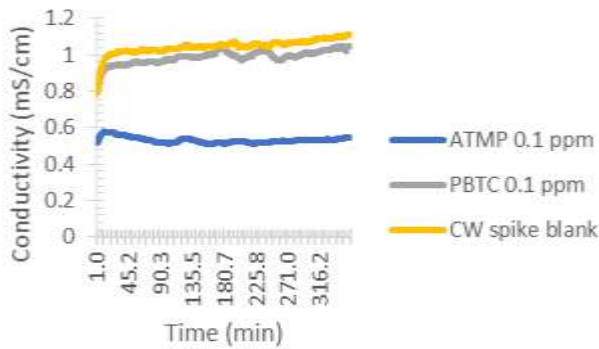


Fig 9: Conductivity over time (CW spike sample 40°C)

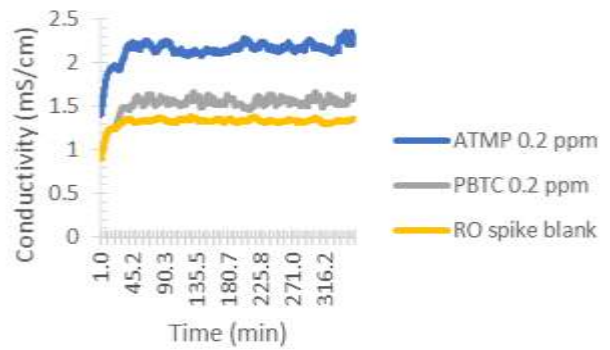


Fig 10: Conductivity over time (RO spike sample 40°C)

At 40°C, there is no observable change in conductivity, and giving rise to the same situation as for 25°C, the control solution and samples are both below super saturation at 40°C to undergo precipitation of CaCO₃.

A graph obtained from the French Creek Modelling application, MineSat™, reveals that the degree of supersaturation for the CW-blowdown and RO-reject stream is relatively low at a temperature of 40°C and a pH 7.4 for CW-Blowdown and pH of 7.8 for RO-reject (Note: the color coding is from Blue which is good to red which is bad and the color can be noted in Fig 11 and Fig 12)

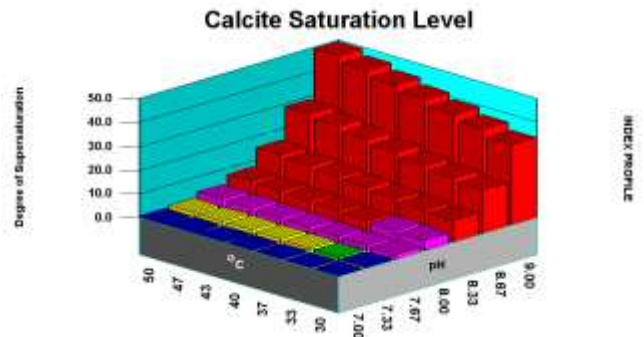


Fig 11: French creek modelling for CW-blowdown sample. Adapted from: French Creek software's MineSat™ [24]

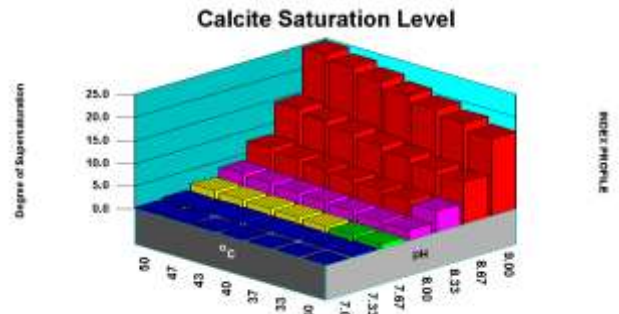


Fig 12: French creek modelling for RO-reject sample. Adapted from: French Creek software's MineSat™ [24]

D. Static induction test at 75°C

Experimental induction tests on the samples and solutions at 75°C produced a diversity of results.

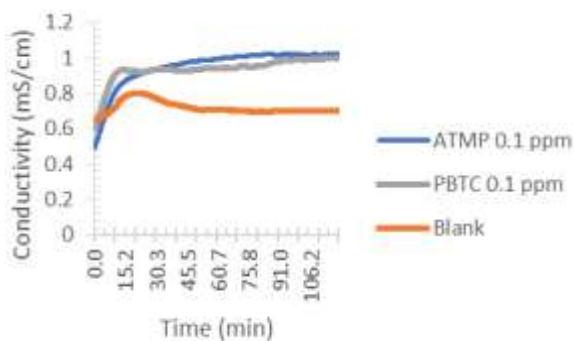


Fig 13: Conductivity over time (Control solution 75°C)

As seen in Fig 13 ATMP performed better than PBTC in terms of induction time for the control solution, as no drop in conductivity occurs for ATMP. The sample containing PBTC shows a very slight decrease in conductivity at 21 min, whereas the decrease in conductivity of the blank is slightly steeper starting at 25 min. The slight decrease in conductivity could be an indication of the occurrence of precipitation, but the drop is not large enough to draw a solid conclusion.

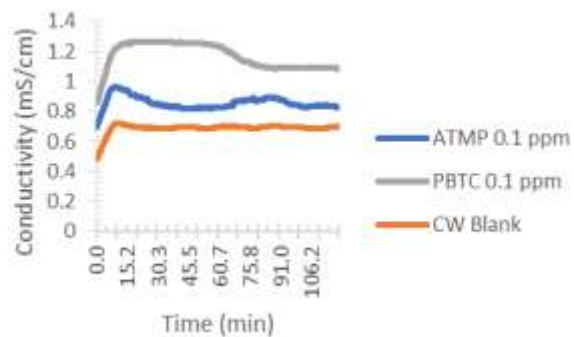


Fig 14: Conductivity over time (CW sample 75°C)

In the case of the CW-Blowdown sample (Fig 14 and Fig 15), it appears that PBTC performs better than ATMP as the conductivity drops much later (62 mins) than that of the ATMP sample (12 mins), while an earlier drop (10 mins) was recorded for the control sample after which the conductivity remained constant for the rest of experiment; it could however be noted that there is no significant difference between the trend observed in the presence of ATMP and the one observed in the control sample.

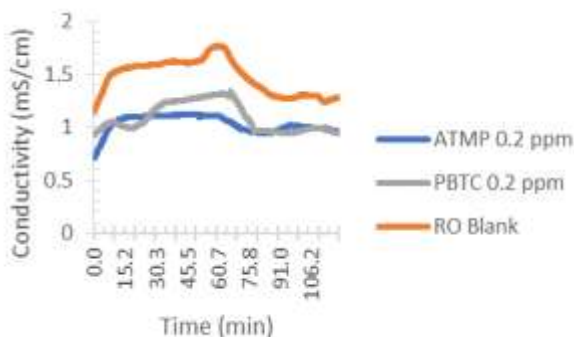


Fig 15: Conductivity over time (RO sample 75°C)

For the RO-reject sample (Fig 15), conductivity appears to decrease before a temperature of 75°C is reached. At high temperatures scaling becomes significant. It can be observed on Figure 15 that all the major drops in conductivity are recorded almost at the same time, although a slight delay by the PBTC could also be identified.

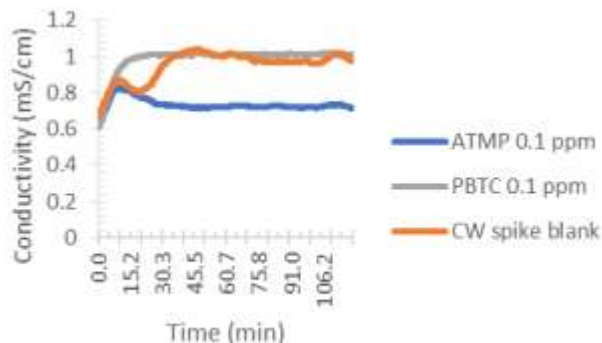


Fig 16: Conductivity over time (CW spike sample 75°C)

In Fig 16 the Blank CW spiked solution shows precipitation at 62°C and 11 mins. ATMP starts a drop in conductivity at 60°C and 12 mins, whereas PBTC shows no drop in conductivity throughout, hence no signs of precipitation.

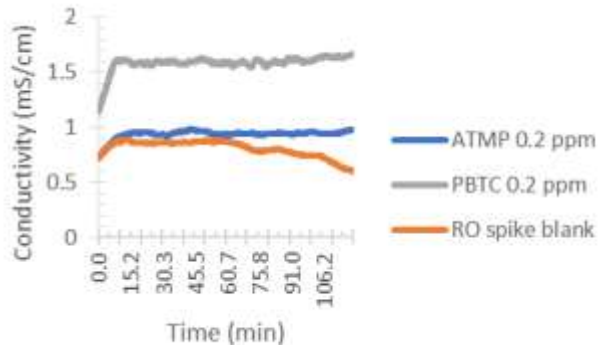


Fig 17: Conductivity over time (RO spike sample 75°C)

The spiked RO-reject sample showed no signs of drop in conductivity for the two considered anti-scalant dosed samples. The blank spiked RO-reject sample started a drop in conductivity at 65 mins.

E. General Discussion

Increasing the rate of heat transfer could allow the prediction of the performance of anti-scalants within reasonable time, as precipitation may be occurring before reaching the targeted temperature. Accurate evaluation of the performance of anti-scalants could be achieved by designing a system that will shorten the heating time required to reach the targeted temperature as in the case on this study precipitation occurred during the heating process, affecting proper evaluation of the performance of anti-scalants.

IV. IMPROVEMENTS

A. Improvement of Testing Method

An improved method of testing the anti-scalants is proposed whereby, a closed jar cylinder is used in place of an open jar. A closed jar can better aid in controlling the temperature and pressure while keeping the contents constant, by overcoming excessive evaporation of water. An accurate and reliable measuring device should be used and more variables should be taken into consideration, such as pH, which can allow to monitor the behaviour of critical elements or compounds in solution such as bicarbonate, carbonate and carbon dioxide content.

V. CONCLUSION

At 25°C there is hardly any change in conditions when temperature of the sample is changed from ambient temperature to 25°C. Conductivity remains constant for all samples, which indicates that the samples are below supersaturated conditions.

After temperatures are reached at 40°C, conductivities remain fairly constant for all samples.

Increasing the temperature to 75°C shows a diversity of trends. In some cases conductivity drops during the initial temperature increase phase, while in others a drop in conductivity was observed only when the targeted temperature was reached. However, in general the anti-scalant PBTC performed better than ATMP both for RO reject water and CW. Overall, it is important to note that in the context of laboratory study aiming to compare the performance of anti-scalants, one must ensure that the solutions considered are supersaturated if results are to be obtained in a short time.

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The corresponding author is currently an Associate Professor in the School of Chemical and Minerals Engineering at the North-West University (Potchefstroom). He is an NRF rated researcher who has published journal articles, book chapters and book.

Prof Elvis Fosso-Kankeu has been the recipient of several merit awards.